



THE STATE
of **ALASKA**
GOVERNOR MICHAEL J. DUNLEAVY

Department of Environmental Conservation

DIVISION OF SPILL PREVENTION AND RESPONSE
Contaminated Sites Program

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Soldotna, Alaska 99669
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www.dec.alaska.gov

File: 2323.38.032

July 14, 2022

Meghan Teegarden
Sr. Advisor, Environmental Remediation
Safety, Health and Environment
Nutrien
5296 Harvest Lake Drive
Loveland, Colorado 80538

Re: UNOCAL/Agrium Ammonia Urea Plant
ADEC Spill # 1988230918305
Biosparge Remediation System Plan – ADEC Review

Ms. Teegarden:

On June 29, 2022, the Alaska Department of Environmental Conservation (ADEC) Contaminated Sites Program received the Biosparge Remediation System Plan, dated June 23, 2022 and prepared by Cook Inlet Environmental.

ADEC has reviewed the document. In future communications please include the name, address, and signature of the Qualified Environmental Professional who prepared the work plan, the name and address of the person who the report is prepared for at Nutrien, and the DEC file number and Hazard ID number on a cover letter. This allows staff unfamiliar with the project to file and respond appropriately.

Figure 4, Cross Section highlights a potential issue with the work plan. The ammonia isolines on Figure 4 are depicted crossing the unsaturated zone of soils below the semi-confining aquitard. This is not a valid method of depicting data. The iso-lines depicting liquid concentrations, cannot cross an unsaturated zone. No soils data has been presented depicting ammonia concentrations. The study *Groundwater Investigation - Interrelationship Between Aquifers and Surface Water Regimes* (Dames & Moore, 1976) highlighted some long-term trends with water table fluctuation at the site. During periods of drought, which we are in currently, the water table fluctuates, rising and falling with changes in precipitation and infiltration.

Since the contamination has moved from the surface through the unconfined to the semi-confined aquifer, we can assume that the aquitard is permeable on site and that the unsaturated soils have been impacted. Not understanding the extent of these unsaturated soils impacts leads to an incomplete conceptual site model, particularly in the source area. With a potential future rise in both the unconfined and semi-confined aquifer water table, additional urea could be mobilized. Understanding and addressing this potential issue now could be

important to the project. Please be aware that future mobilization of urea in the presently unsaturated aquifer, caused by a rise in the water table could delay site remediation.

Were unsaturated soils sampled to completely characterize source area impacts to the unsaturated zone? Was any consideration given to remediation alternatives in the unsaturated zone?

The work plan is approved. If there are any questions, please contact me at (907) 262-3412 or by e-mail at peter.campbell@alaska.gov.

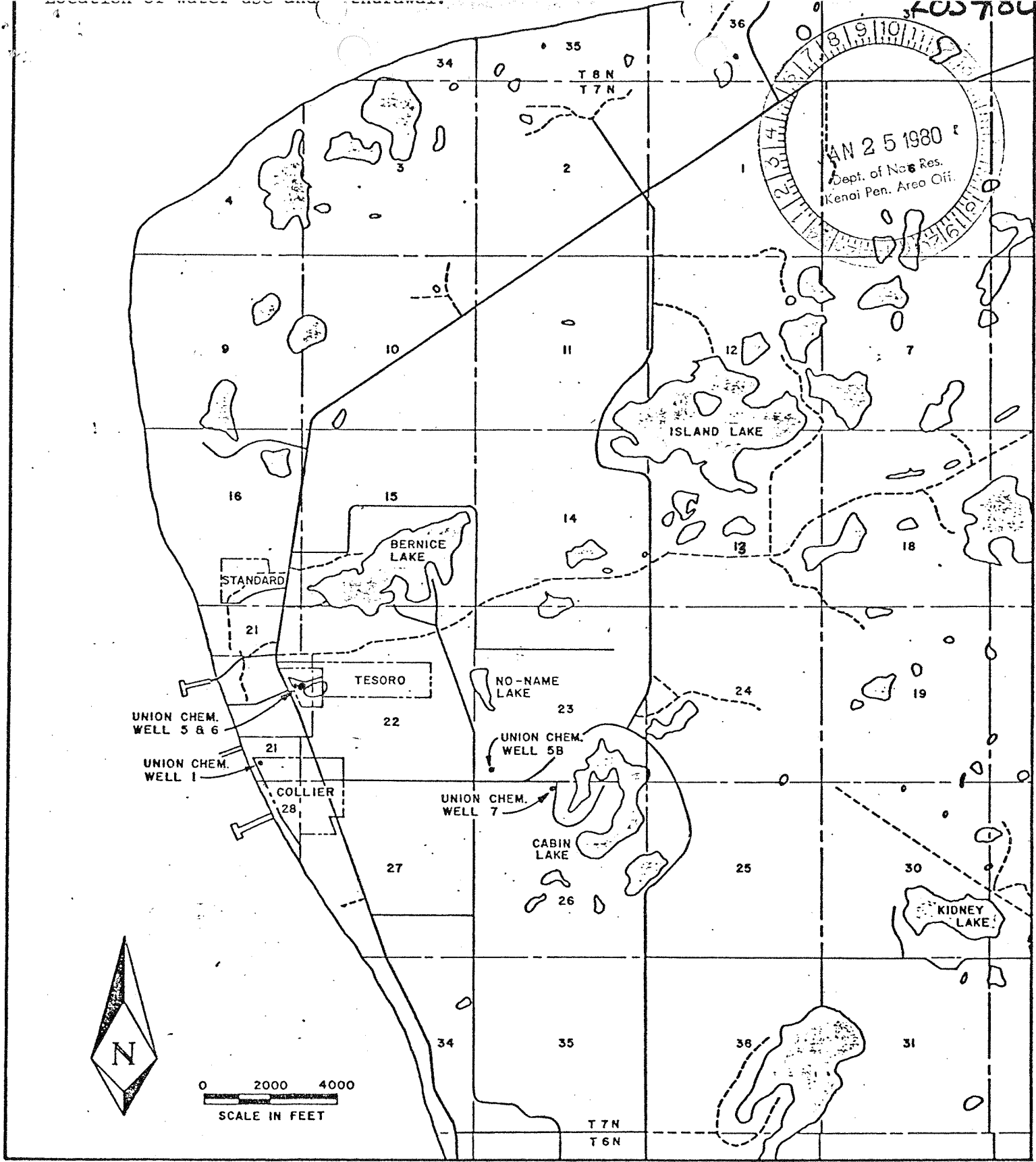
Sincerely,

Peter Campbell

Peter Campbell
Environmental Program Specialist

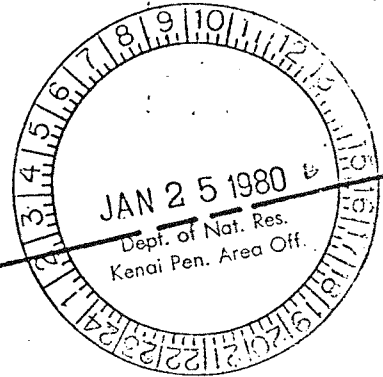
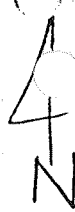
C: Electronic copies:
Jene' Worley - Cook Inlet Environmental
Lisa Krebs-Barsis – ADEC

Attachment: [Groundwater Investigation - Interrelationship Between Aquifers and Surface Water Regimes \(Dames & Moore, 1976\)](#)

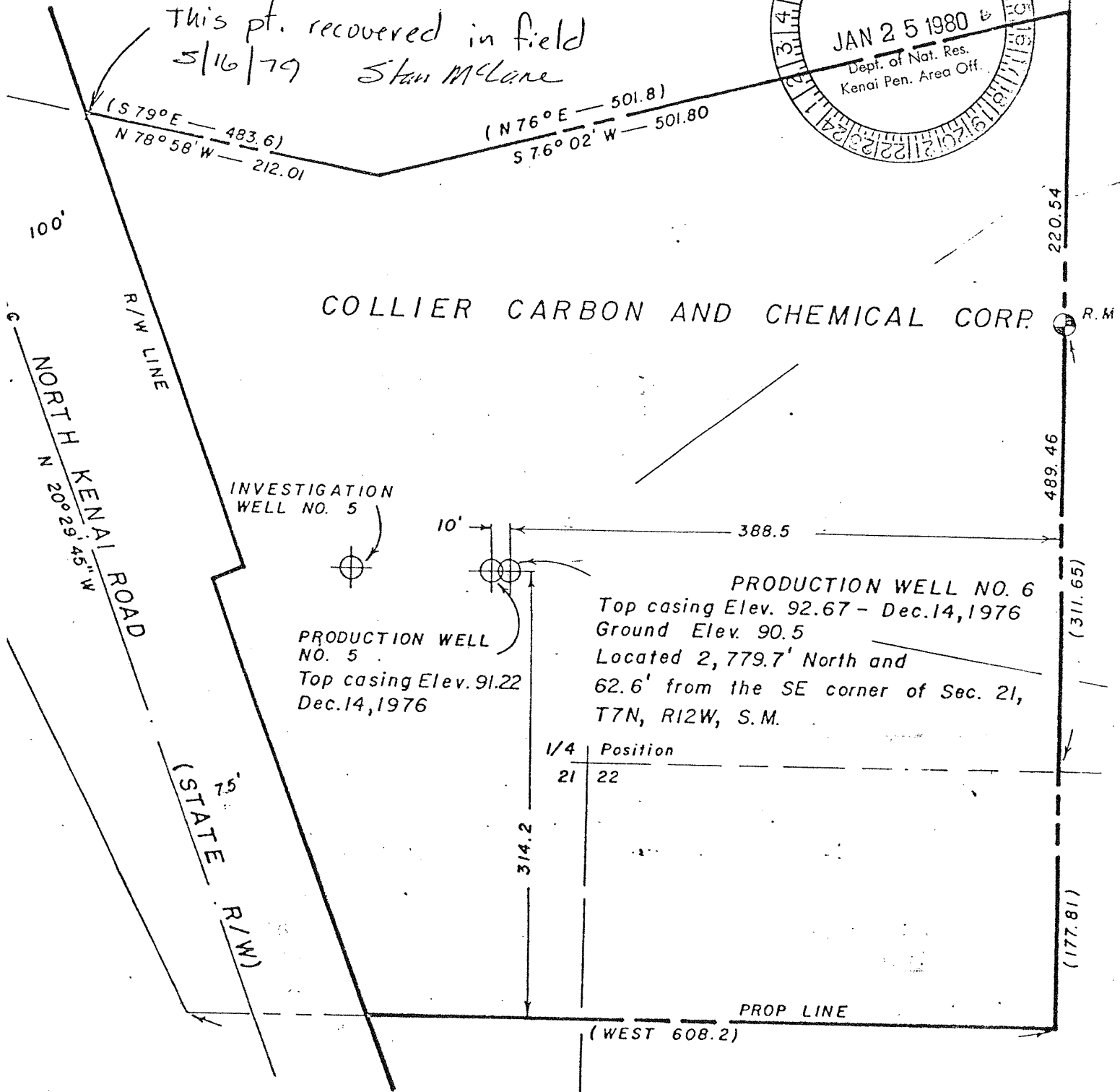


VICINITY MAP

FIGURE NO.



This pt. recovered in field
5/16/79 Stan McLane



COLLIER CARBON AND CHEMICAL CORP.

INVESTIGATION WELL NO. 5

PRODUCTION WELL NO. 5
Top casing Elev. 91.22
Dec. 14, 1976

PRODUCTION WELL NO. 6
Top casing Elev. 92.67 - Dec. 14, 1976
Ground Elev. 90.5
Located 2,779.7' North and
62.6' from the SE corner of Sec. 21,
T7N, R12W, S.M.

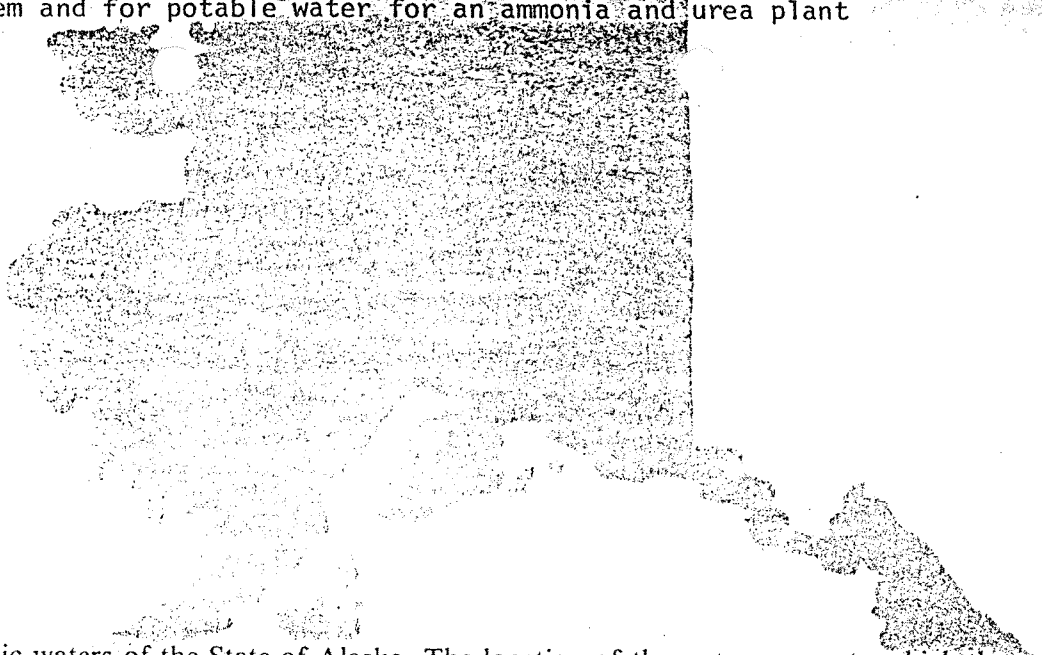
1/4 Position
21 22

PROP LINE

(WEST 608.2)

21	22
28	27

steam system and for potable water for an ammonia and urea plant

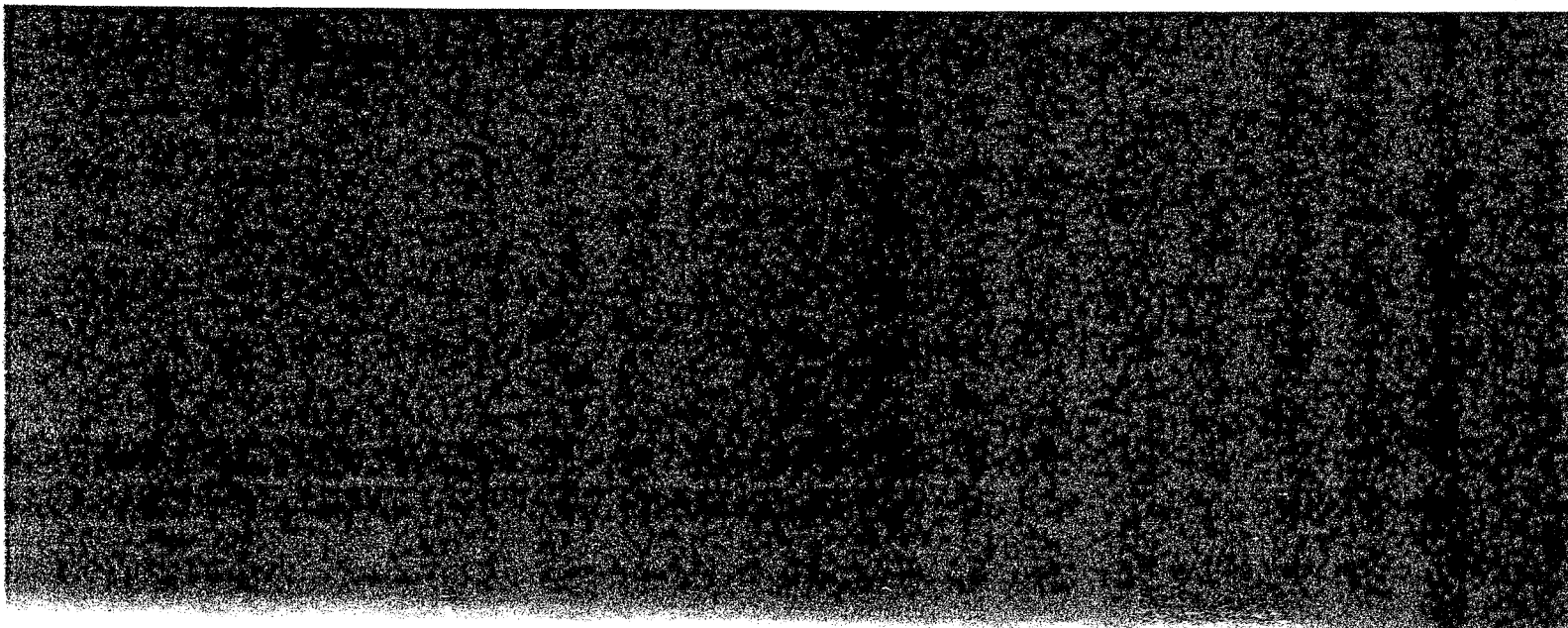


from the public waters of the State of Alaska. The location of the water source to which the water right granted appertains is a drilled well, 160 feet deep (PW #6), within that portion of Tract Two (2) as shown on Homestead Entry Survey No. 74 (new No. U.S. Survey 1095) according to Plat K-672 which is described as follows:

location
MAB

Starting at Corner No. 4 of Homestead Entry Survey No. 74 (U.S. Survey No. 1095), go North 1140 feet, the True Point of Beginning and Corner No. 1; thence West 608.2 feet to the intersection with the Kenai Boulder Point Road and Corner No. 2; thence North $23^{\circ}30'$ West a distance of 457.4 feet to Corner No. 3; thence North $26^{\circ}45'$ West a distance of 310.9 feet to Corner No. 4; thence South 79° East a distance of 483.6 feet to Corner No. 5; thence North 76° East a distance of 501.8 feet to Corner No. 6; thence South along the East boundary of Homestead Entry Survey No. 74, (U.S. Survey No. 1095), a distance of 710 feet to Corner No. 1, said parcel of property located within Sections 21 and 22, Township 7 North, Range 12 West, Seward Meridian.

insy
LS 8-28-80
ESP
8-27-80
C.K.



WATER WELL 150 SITE ID 604102151224702

LOCAL NO. SB7-12-21-ADDD 2-9

(1) OWNER: NAME COLLIER CARBON & CHEMICAL ADDRESS KENAI, ALASKA

(2) LOCATION OF WELL: COUNTY: OWNER'S NUMBER, IF ANY: PROD. WELL KENAI BOROUGH NEAR NIKISKI, ALASKA 2,779.7' NORTH & 62.6' WEST OF SE CORNER OF SEC. 21, T7N, R12W, SEWARD MERIDIAN. GROUND ELEV. 90.5 MLLW DATUM

(3) TYPE OF WORK (check) NEW WELL [X] DEEPENING [] RECONDITIONING [] ABANDON [] IF ABANDONMENT, DESCRIBE MATERIAL AND PROCEDURE IN ITEM 11.

(4) PROPOSED USE (check) DOMESTIC [] INDUSTRIAL [X] MUNICIPAL [] IRRIGATION [] TEST WELL [] OTHER [] (5) EQUIPMENT: ROTARY [] CABLE [X] DIG WELL []

Table with columns for casing installed (single/double), gage or wall, diam. of rope, from ft., to ft., and size of gravel. Includes description of joint: 3 BEAD WELD.

Table for perforations or well screen: stainless steel-16" telescopic. Includes size of perforations (slot) and length in inches.

(8) CONSTRUCTION: WAS A SURFACE SANITARY SEAL PROVIDED? YES [X] NO [] TO DEPTH FT. WERE ANY STRATA SEALED AGAINST POLLUTION? YES [] NO [] DEPTH FT.

METHOD OF SEALING

(9) WATER LEVELS: DEPTH AT WHICH WATER WAS FIRST FOUND 23, 101 FT. STANDING LEVEL BEFORE PERFORATING FT. STANDING LEVEL AFTER PERFORATING FT. PIEZOMETRIC ARTESIAN HEAD @ 61.8' WAS A PUMP TEST MADE? YES [X] NO [] IF YES, BY WHOM? DRILLER YIELD: 1200 GAL./MIN. WITH 31.6 FT. DRAWDOWN AFTER 48 HRS. TEMPERATURE OF WATER WAS A CHEMICAL ANALYSIS MADE? YES [X] NO [] WAS ELECTRIC LOG MADE OF WELL? YES [] NO [X]

Table for well log: TOTAL DEPTH 160 FT. FORMATION: DESCRIBE BY COLOR, CHARACTER, SIZE OF MATERIAL AND STRUCTURE. Includes depth intervals and formation types like DRY GRAVEL, CSE SAND, GRAVEL-PLENTY, WATER, FINE-MED. SAND, SOLID BLUE CLAY, SOME LARGE ROCK, CSE GRAVEL, CSE SAND & GRAVEL, 30% GRAVEL, MED.-CSE SAND, 50% GRAVEL (CSE), CSE SAND & SMALL GRAVEL, SMALL, MED. CSE. GRAVEL W/CSE. SAND, VERY CSE SAND W/10% GRAVEL, VERY CSE SAND GRADING TO FINE.

WORK STARTED 1976. COMPLETED 1976

WELL DRILLER'S STATEMENT: THIS WELL WAS DRILLED UNDER MY JURISDICTION AND THIS REPORT IS TRUE TO THE BEST OF MY KNOWLEDGE AND BELIEF.

NAME (PERSON, FIRM, OR CORPORATION) (TYPE OR PRINTED) ADDRESS (Signed) J. J. SHELMAN (WELL DRILLER) SOLDATNA DRILLING

ADDD 2-9

SD 1-18-21-ADDD 2-9

Well Identification Number PRODUCT# WELL #6

Potable Water System Well

Drilling Co. Soldotna Drilling USGS no. _____

Driller J. Shellman Type of rig Cable Date well completed 8/76

Well owner _____ Nearest community Kenai

Well location: (address & legal description 2779.7' North & Longitude 1512247

62.6' W of S.E. Corner of Sec. 21, T7N, R12W Latitude 604102

Depth of well 160 ft. Casing: Depth 151 ft. Diameter 16 in.

Static water level 61.8 ft. (above, below) land surface. Date _____

Finish of well: (open end, screen, perforated, open hole, other) Stainless

Describe screen intervals and size: 101-136" = 0.125 Slot 136-151 = 0.035 Slot

Well yield tested by (pumping, bailing, air) at 1200 gal/min.

for 48 hours with 31.6 ft. of drawdown from static level.

DRILLER'S MATERIAL LOG

Depth below land surface in feet	Give description of strata penetrated (size of material, color, hardness of drilling, and water content)
0 to 23	Dry Gravel
23 to 71	Coarse Sand & Gravel-Plenty of Water
71 to 77	Fine to Medium Sand
77 to 101	Solid Blue Clay Some Large Rock
101 to 109	Coarse Gravel
109 to 114	Coarse Sand & Gravel 30% Gravel
114 to 124	Medium-Coarse Sand- 50% Coarse Gravel
124 to 128	Coarse Sand & Small Gravel
128 to 136	Small, Medium, Coarse Gravel with Coarse Sand
136 to 139	Very Coarse Sand with 10% Gravel
139 to 160	Very Coarse Sand Grading to Fine
to	
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REPORT
GROUND WATER INVESTIGATION
INTERRELATIONSHIP BETWEEN AQUIFERS AND
SURFACE WATER REGIMES
NORTH KENAI AREA, ALASKA
FOR COLLIER CARBON AND CHEMICAL CORPORATION

GM INVESTIGATION
DESIGNED BY GUYTON
AQUIFERS / SURFACE WATER

EO
AN
RLM - LA
JRM - BR
AM - CR
WAT - AN
WAE - AN
RPB - AN

DAMES & MOORE
JOB NO. 4828-016-20
MAY 28, 1976

SUMMARY

The adequacy of existing areal and historic hydrologic data is limited. The U.S. Geological Survey (USGS) is the primary source of data.

Numerous well logs are available but are scattered over wide areas. Many domestic well logs have not been filed with the State of Alaska or the USGS.

Lakes and swamps in the North Kenai region contain large quantities of water. A large proportion of the lakes are part of the general water table. Annual and long-term variations in precipitation are the principal causes of fluctuations in the water levels.

Surface runoff, over most of the North Kenai area, is minimal. In the North Kenai ground water basin, only Bernice Lake has a visible outlet to Cook Inlet. Sources of runoff are snowmelt and rain.

Streams draining the northeast portion of the North Kenai area are Bishop Creek and Beaver Creek. Both have sustained flow, receiving discharge from lakes and ground water.

The water-bearing deposits underlying the study area are glacial outwash deposits and drift of Quaternary age.

Ground water supplies are abundant in the North Kenai area. Two aquifer systems are present -- unconfined water table aquifers and the deeper confined artesian aquifers. The water table aquifer water is high in iron and much of the artesian water in deeper aquifers contains tanin and lignin.

Water use during 1975 is estimated to be on the order of 1,100 million gallons, entirely supplied from wells. Of this amount, industry is estimated to have pumped 950 million gallons during 1975.

Precipitation and seepage from lakes are the principal sources of recharge to the water table aquifers. Precipitation is the principal source of recharge to the artesian aquifers. Precipitation at the Kenai Airport averaged 18.97 inches over the 30-year base period (1945-1975).

Evapotranspiration, pumping and flow of aquifer water to Cook Inlet account for large quantities of ground water discharge.

Based on USGS measurements of high water marks in lakes, the water level has declined as much as 6 feet. This is primarily due to drought conditions and evapotranspiration.

The hydrostatic head of the artesian aquifer has been reduced approximately 6 feet since 1967 due to pumping and reduction of recharge during periods of low precipitation. Indications are that the artesian water level started to stabilize during 1975.

Chemical analyses indicate the water table aquifer to be much higher in iron than the artesian aquifer. A low iron concentration has remained constant in the artesian aquifer.

Hydraulic characteristics of aquifers of the North Kenai area are highly variable. There are high variances in transmissivity, storage characteristics and hydraulic conductivity.

A 5-year drought period occurred during 1946-1950 with another drought starting in 1968 and continuing through 1975. The surface water drainage basins in the North Kenai area have had an estimated net loss, related to precipitation, of 45,080 acre-feet of water for the period 1968-75.

A photogrammetric study of five lakes and evaluation of USGS data indicated that water level elevations in the North Kenai area were at very high levels in 1963. These data indicate that between 1963 and 1968 most lake levels in the area dropped about 3 to 4 feet. This water level lowering may have been due to water seeking its long-term natural level or a consequence of the 1964 earthquake. Further decreases occurred during the extreme drought period of 1968 and 1969. Since 1970, lake levels have had no large changes despite the low level of rainfall. Available information indicates that Cabin Lake dropped about 3.3 feet during the period between 1963 and late 1968 and dropped another 3 feet by late 1974. Since late 1974, the lake has raised about 1 foot.

Computer modeling results indicate that approximately 3.7 feet of water level reduction in the Cabin Lake area has occurred between late 1968 and late 1974 (correlating reasonably well with 3 feet of reduction indicated above). The primary cause of this drop may be attributed to the severe drought of 1968 and 1969 in combination with a succession of years of below normal precipitation. Other causes, including residential and industrial pumping, may be responsible for additional reductions. Because the Cabin Lake level has remained essentially constant since 1971, a period when precipitation was below normal every year, it is doubtful that pumping reduced the lake level significantly. The correlation between

measured lake level reduction and the computer results are considered to be reasonable. Further attempts at exact duplication of historical data are impractical.

Results of the computer simulation indicate that about 15 percent of approximately 2.5 feet, or 0.4 feet, of lake level drawdown since Collier started pumping in late 1968 may be attributed to the pumping activities. Photogrammetric data indicate that an additional 2.5 to 3 feet of water level decline occurred prior to the start of Collier's pumping activities.

It is our opinion that water level loss due to pumping is minor when compared to the overall losses in the water resource region. It is also our opinion that water levels may continue to be reduced unless natural recharge in the area return to levels that are normal or above normal.

GENERAL CONCLUSIONS

Ground water is abundant in the North Kenai area even though drought conditions have persisted since 1968. The lowering of the water table and lake levels is principally due to lack of precipitation and, consequently, reduction of recharge to lakes and aquifers. Although contributing to these conditions, withdrawals from water wells are a less significant factor.

The seemingly stabilized water levels and apparent reversal of downward trends during 1975 may indicate that discharge is no longer exceeding recharge. However, continuation of drought conditions and increasing localized withdrawals of ground water are of concern. Pumping from water table aquifers has a direct effect on lake levels. Proper planning and management of water resources and continued monitoring of water levels and water usage can avert adverse effects on the hydrologic systems. Pumping from deeper confined aquifers will minimize any possible effects on lake levels.

TABLE 1

SUMMARY OF LAKE LEVELS IN KENAI AREA, ALASKA^a

Lake Name	Summer 1970	7/13&14 1971	10/13 1971	6/22&23 1972	9/28 1972	10/18 1973	10/15 1974	10/13&14 1975
(No name) Sec. 23 T7N R12W	10.17	9.43	9.87	10.33	10.54	10.25	9.08 ^b	10.55
Cabin	11.29	10.47	10.22	10.68	10.63	10.52	9.25	10.29
Bernice	16.95	16.64	16.72	17.45	17.53	17.95	16.90	17.54
Island	10.10	10.15	10.67	11.36	11.66	11.61	10.41	11.19
Dogbone	4.96	4.65	4.64	5.24	5.11	5.17	4.45	5.02
Kidney	10.43	10.78	11.31	11.67	12.02	11.60	10.83	12.22
Wick	13.08	13.54	14.10	14.91	15.09	14.97	14.18	15.41
Douglas	14.12	14.19	14.37	15.00	15.17	15.18	--	15.79
Laura	2.25	2.62	3.23	4.15	4.34	4.37	3.61	4.71
Konovalof	14.72	14.95	--	--	--	--	--	17.07
Shadura	15.00	15.60	--	--	--	--	--	16.50
Daniels	16.86	16.82	--	--	--	--	--	17.53

^aSource: U.S. Geological Survey, arbitrary reference point.
^bRevised 1975.

TABLE 2

INDUSTRIAL GROUND WATER USAGE

(Yearly Total Gallons x 10⁶)

User	<u>1967</u>	<u>1968</u>	<u>1969</u>	<u>1970</u>	<u>1971</u>	<u>1972</u>	<u>1973</u>	<u>1974</u>	<u>1975</u>
Collier Carbon	--	92.0	501.0	549.2	526.0	599.0	571.0	599.0	586.0
Phillips Petroleum	--	--	33.4	156.0	167.0	193.0	154.0	163.0	192.0
Tesoro	--	--	6.3	72.2	73.0	80.0	100.0	65.0	72.0
Standard Oil	52.6 ^a	52.6 ^a	52.6 ^a	53.0 ^b	53.0 ^b	53.0 ^b	53.0 ^b	53.0 ^b	53.0 ^b
Rig Tenders	281.0	242.4	123.4	70.2	48.0 ^a	48.0	48.0	48.0 ^b	30.0 ^b
Chugach Electric	15.8	15.8 ^a	15.8 ^a	15.8	16.0 ^b	16.0 ^b	16.0 ^b	16.0 ^b	16.0 ^b

^aEstimated by USGS.^bEstimated by Dames & Moore.

TABLE 3

DOMESTIC WATER USE, NORTH KENAI AREA

<u>Year</u>	<u>Estimated Population</u> ^a	<u>Ground Water Use</u> <u>(million gallons/year)</u> ^b
1968	2,500	91.2
1970	2,800	102.2
1975	3,100	113.2

^aPopulation estimate from the Kenai Comprehensive Plan, Alaska State Housing Authority, 1969.

^bBased upon 100 gpd/person.

HYDROLOGIC SETTINGSURFACE WATER AND DRAINAGE

The hydrology of the North Kenai region is controlled by the climatic and terrain features. Topographic relief is variable, ranging from low, swampy areas to the undulating morainal deposits. Streams are generally small and meander through extensive swamp and muskeg areas. With the exception of Bishop Creek, the streams are generally short and discontinuous. Drainage basin boundaries are difficult to define due to the low relief and isolated lakes. However, surface water basin boundaries have tentatively been delineated and divided into major and minor basins by Anderson and Jones (1972) and modified by Dames & Moore for this report (Figure 3). Drainage areas of selected basins have been calculated by planimeter and are presented in Table 5. The area measurement of Bishop Creek surface water basin, as indicated on Figure 3, was terminated at the northernmost boundary of USGS topographic map sheets Kenai C-3 and C-4. Bishop Creek is a perennial stream and drains northward to Cook Inlet. The mean annual peak discharge from streams draining the low swamps east of Nikiski average about 1 cfs per square mile. The mean annual low runoff at Nikiski averages about 0.5 cfs per square mile (Feulner, Childers, and Norman, 1971).

Lakes and swamps in the North Kenai region contain large quantities of water. Some small lakes are perched on relatively impermeable silt above the water table, while others fill topographic lows and are a part of the general water table. Annual and long-term variations in precipitation cause water levels of some lakes to fluctuate considerably.

Most lakes within the study area are closed basins or seepage lakes. That is, there is no visible inlet or outlet to the lake, but ground water enters and leaves by seeping through the confines of the lake basin. Cabin, Wick, and Douglas Lakes are examples of closed basin or seepage lakes. Other lakes, such as Bernice, Salamatof, and Daniels have outlets but no visible inlet; these are semi-closed lake systems.

GROUND WATER

Assumed ground water basin boundaries have been developed by the USGS corresponding with either surface water drainage or known impermeable subsurface boundaries. The areas of the ground water basins are presented in Table 6. The basins are indicated on Figure 4. Confined and unconfined ground water aquifers are found over much of the North Kenai area.

Four subsurface geologic sections (Figures 5 through 8) have been compiled from existing well and boring log information. Location of the sections are indicated on Plate 2 (in pocket). The wells are too few and widely spaced in some areas to accurately map the subsurface units and the static surfaces of the water table and artesian aquifers. Broad correlations between the well locations are the basis for a description of general stratigraphy.

To depths of approximately 300 feet, four major stratigraphic units are present. The upper unit consists of outwash sand and gravel in thin alternating discontinuous layers which occur to depths of 125 feet below the surface. In this unit, ground water occurs under water table conditions. The depth to water in the water table aquifer, as indicated in the subsurface sections, varies between 5 and 70 feet below land surface.

Near the Cook Inlet bluffs, the surface of the static water table decreases in elevation and appears at the surface near the base of the sea cliff.

Beneath the upper sand and gravel unit is a confining stratum consisting of clay and silt which locally alternates with thin layers of silty sand and sand. The clay stratum varies in thickness from 5 to 40 feet and appears to pinch out beneath the Collier plant site near the Cook Inlet bluffs (Figure 6). The clay stratum also appears to pinch out to the north of the plant site in the vicinity of Bernice Lake (Figure 7).

Beneath the clay stratum, which acts as a confining layer to the artesian ground water, are more variable strata consisting of silty sand containing coal fragments interbedded with discontinuous strata or lenses of water bearing sand and, more rarely, gravel. The sand and gravel aquifers, being discontinuous, are difficult to locate but are differentiated in the subsurface sections where possible, as the third geologic unit. North of the plant site toward Bernice Lake, the silty sand grades to poorly graded sands and gravels with fewer fines.

In the deeper wells and borings, a second (lower) clay stratum is encountered at depths of 170 to 240 feet below the surface. The clay is interbedded with thin layers of sand and gravel containing water under artesian conditions. The lower clay unit varies in thickness from 60 to 130 feet and was encountered in borings drilled to a maximum depth of 450 feet below the ground surface.

Recharge

Water table aquifers of the North Kenai area are recharged primarily by precipitation and seepage from lakes. Most of the area studied lies in a

soils region of good recharge potential. The region encompasses well-drained soils underlain by glacial drift. Precipitation is the principal source of recharge to the confined aquifers, although the major portion of water contribution is considered to originate east of the area of study. Data on the area to the east is extremely scarce or non-existent.

Based upon climatological, vegetated area, and soils data, net recharge from normal amounts of precipitation is estimated to range from 7 to 9 inches per year. Ground water underflow, entering the study area from the east, is also a contributing recharge factor. The flow rate is not known but is believed to be slow due to barriers of low permeabilities and gentle water table gradient.

Discharge

Ground water of the water table aquifer in the North Kenai area is discharged primarily by evapotranspiration, pumping, and seeps and/or springs from the coastal bluffs.

Discharge from the artesian aquifer occurs by pumpage and upward movement of the water through semi-confining beds where the artesian water level is higher than the water table aquifer. It is generally believed that artesian aquifers discharge large quantities of water into Cook Inlet.

Total evapotranspiration for the North Kenai area is estimated to be on the order of 5 to 10 inches per year, due to the high percentage of forested area and the numerous bodies of lake water. Although total ground water loss through evapotranspiration is not known, it is considered to be a significant portion of the total evapotranspiration.

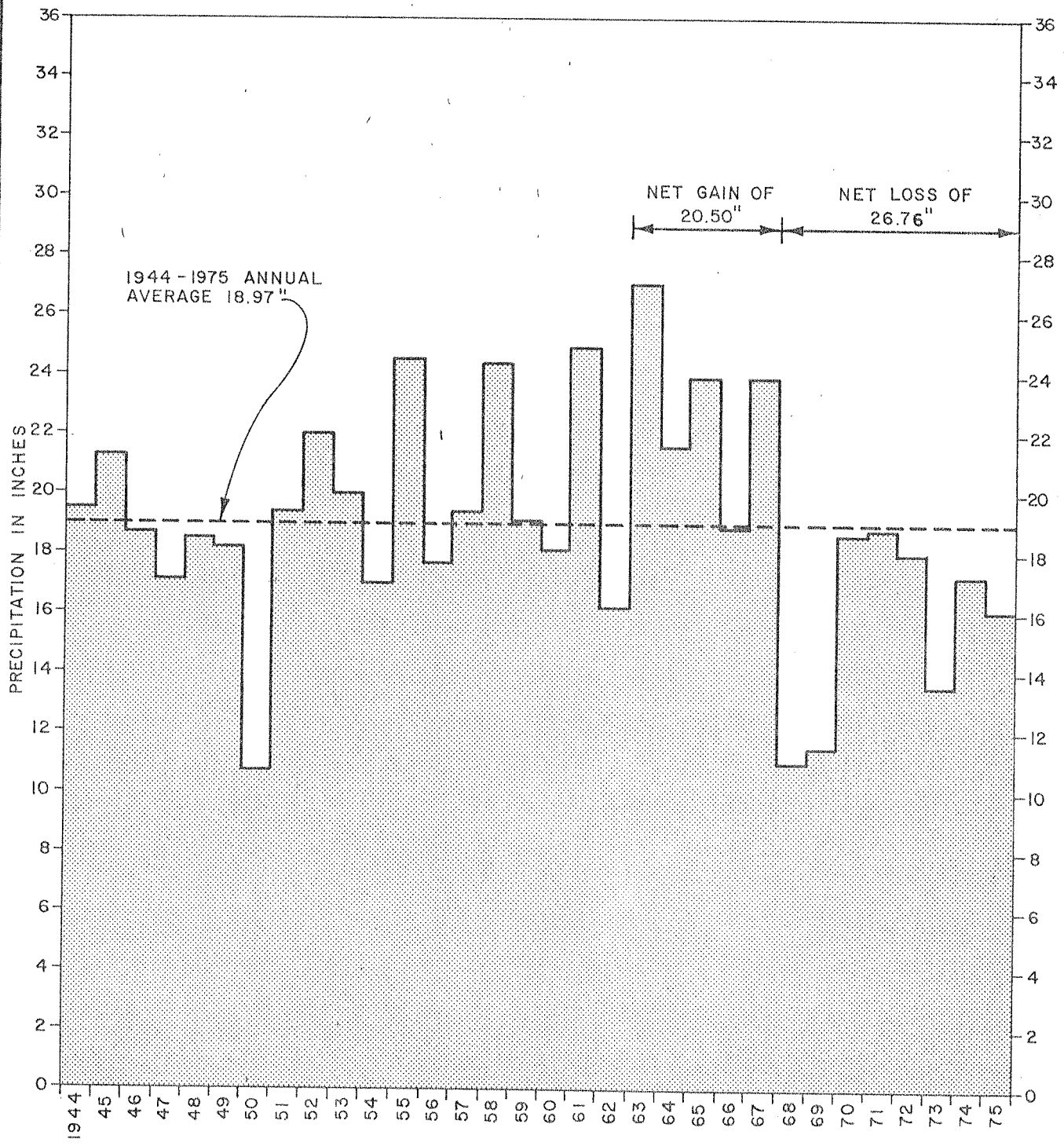
Pumpage of ground water in the system consumes an estimated 2.9 mgd.

Water Level Fluctuations

Fluctuation of water well levels are indicated on Figure 9 for an artesian aquifer and a water table aquifer in the North Kenai area. Water level fluctuations can be caused externally by tidal movements, changing atmospheric pressures, wind over an open well, and by earthquakes. Internally, varying amounts and rates of recharge and discharge will cause water level fluctuations.

Review of available hydrographs indicate that the water table aquifer responds to seasonal changes. The aquifer reaches its highest levels in August, September, and part of October. Once the ground freezes, there is about 6 to 7 months' lag time before winter precipitation percolates to the water table. The water levels reach their lowest point during February or March. Based on USGS hydrographs, the water level of the water table aquifer has varied as much as 5 feet (see Figure 9). This is primarily due to natural causes such as evapotranspiration and drought conditions.

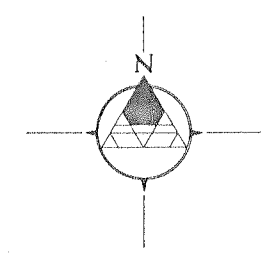
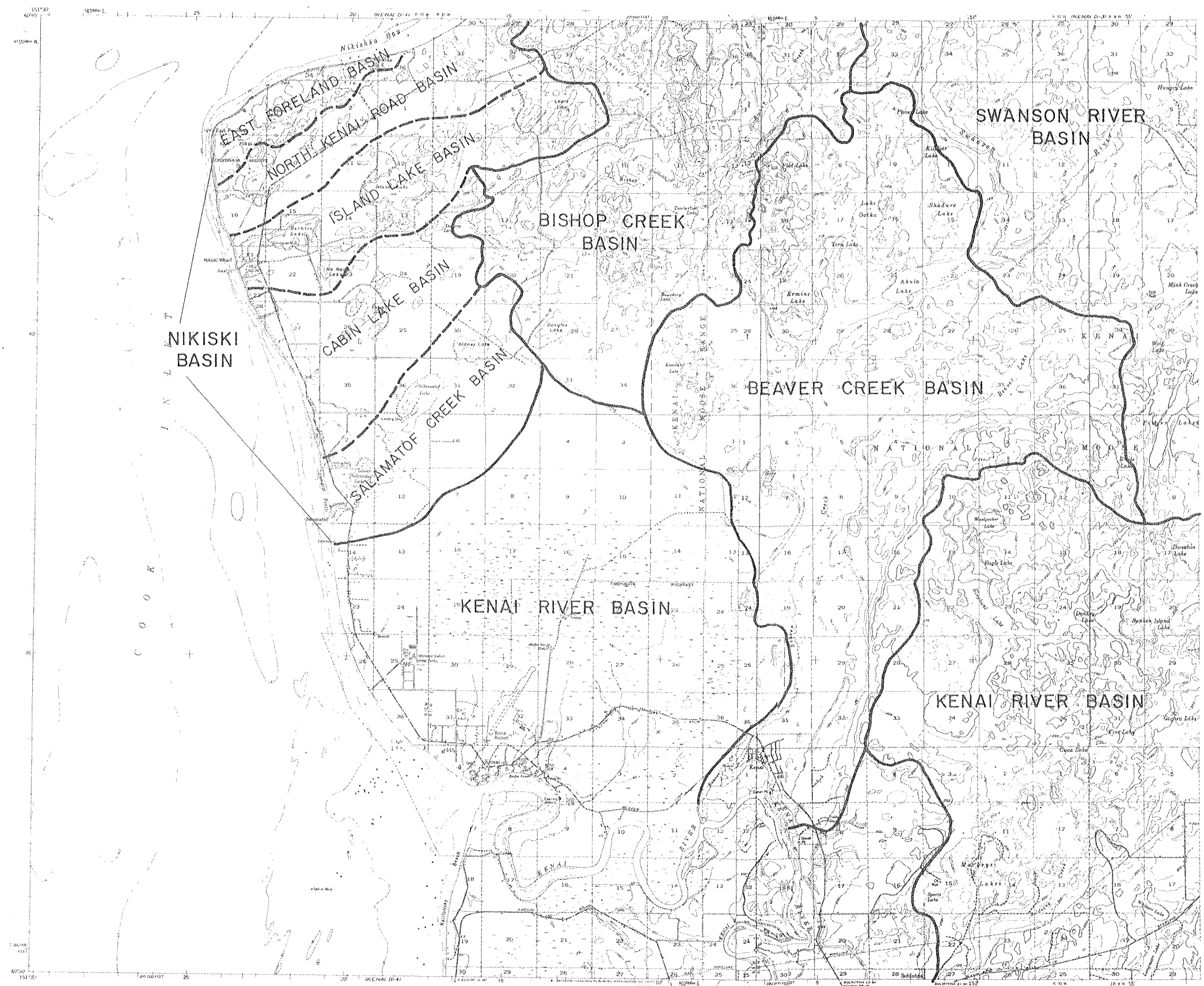
Artesian aquifers generally have a greater lag time in their response to precipitation. Under drought conditions, the amount of recharge is reduced also to the artesian aquifer. Fluctuation of water levels under artesian conditions are primarily caused by changes in pressure rather than changes in storage volume. The confined aquifer serves mainly as a conduit for moving water from recharge areas to locations of natural or artificial discharge. Reduction of recharge and increased pumpage have caused the



**ANNUAL PRECIPITATION
 AT KENAI MUNICIPAL AIRPORT
 1944-1975**

REFERENCE :
 U.S. ENVIRONMENTAL DATA SERVICE,
 1944-75. CLIMATOLOGICAL DATA-ALASKA,
 NATIONAL CLIMATIC CENTER, ASHEVILLE, N.C.

DAMES & MOORE



KEY

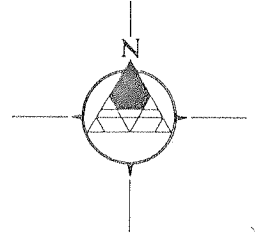
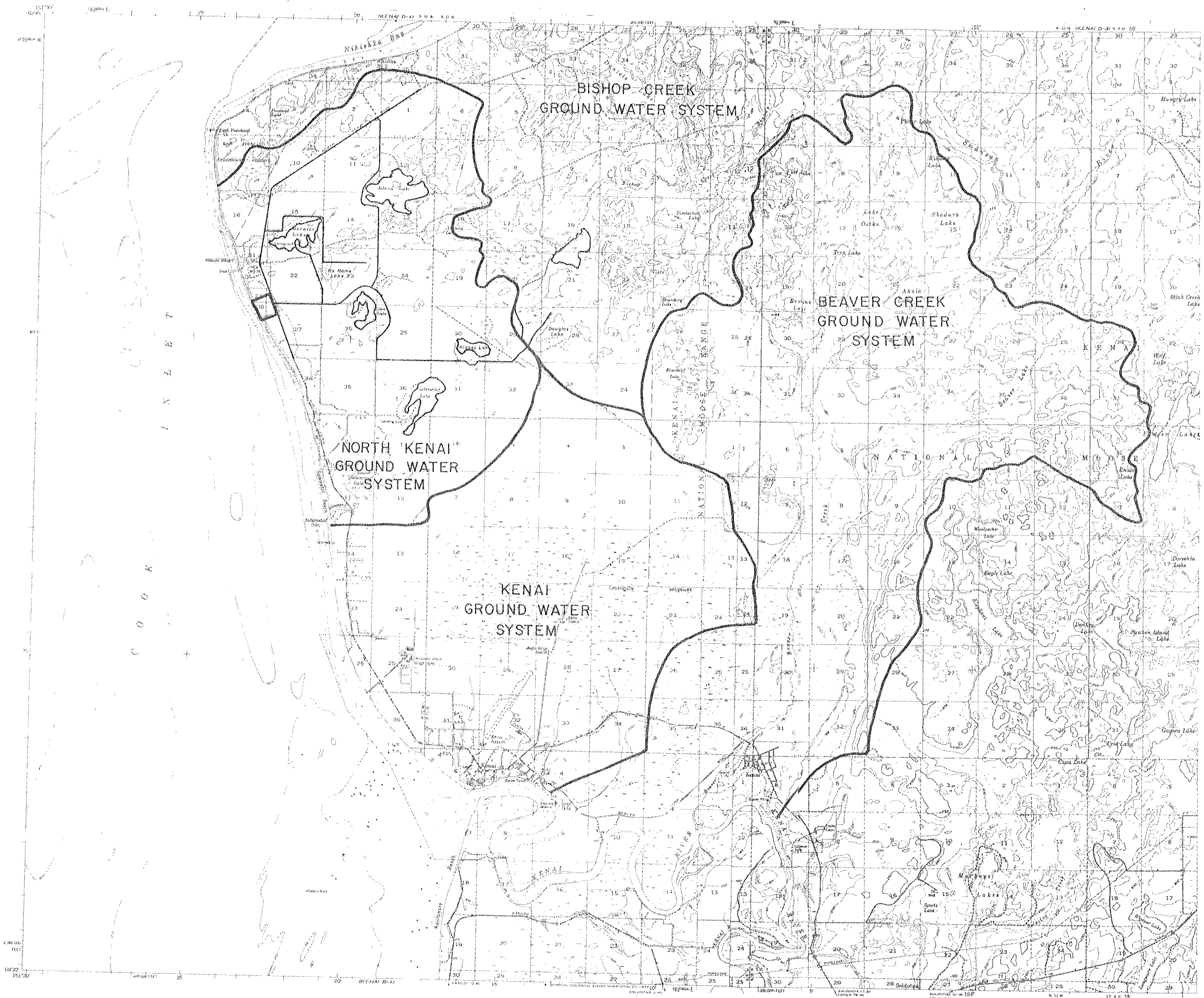
———— MAJOR BASIN BOUNDARY

----- SUB-BASIN BOUNDARY

**SURFACE WATER
DRAINAGE BASINS**



REFERENCE:
ANDERSON & JONES, 1972
MODIFIED BY DAMES & MOORE, 1976



KEY

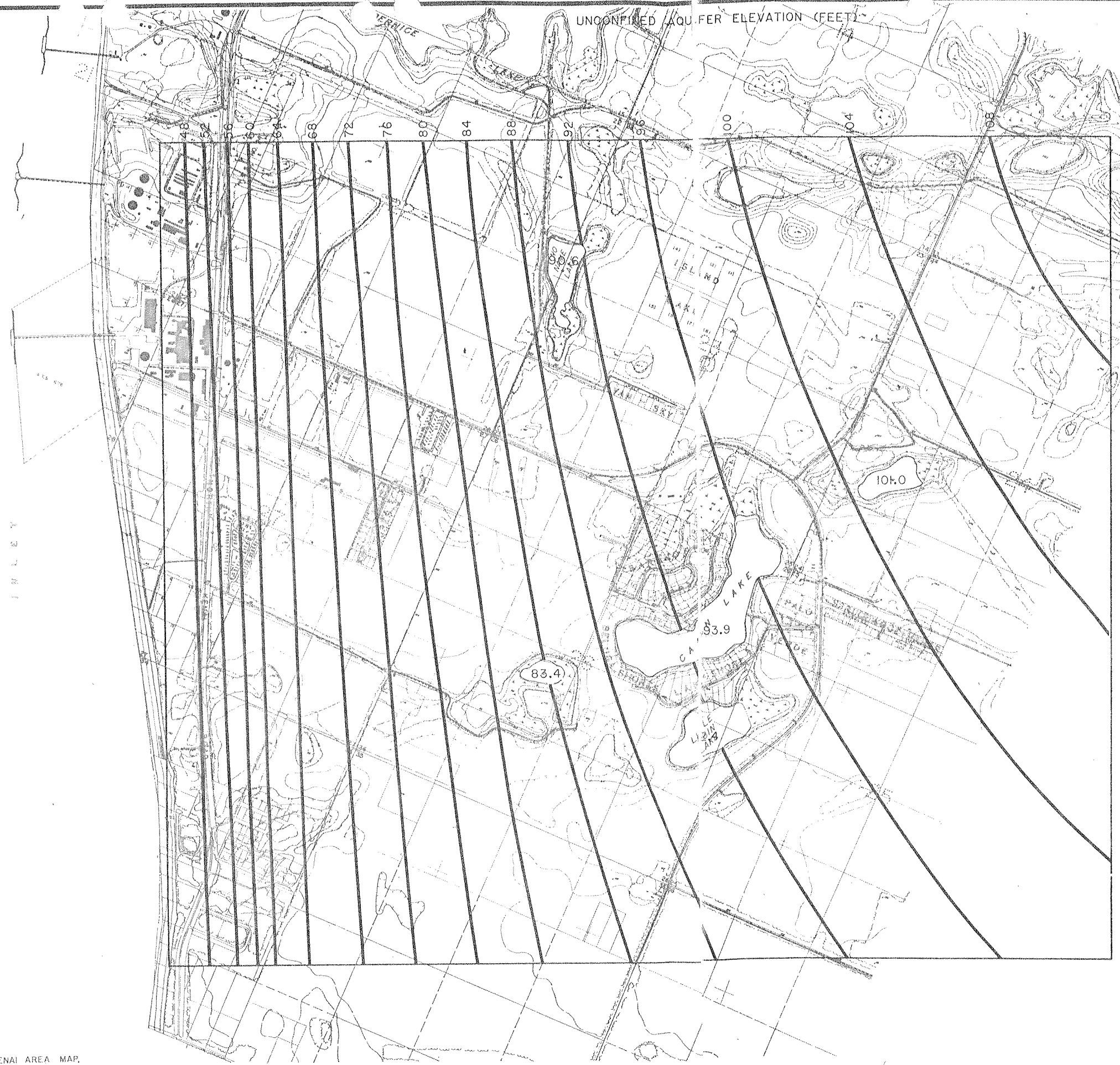
———— BASIN BOUNDARY

GROUND WATER BASINS



REFERENCE:
ANDERSON & JONES, 1972

UNCONFINED AQUIFER ELEVATION (FEET)



NOTES

1. TIME FROM START OF COMPUTER SIMULATION, MAY 1, 1965: 3717 DAYS
2. PUMPING; LEAKY BOUNDARY
3. RECHARGE = 40% ACTUAL ANNUAL PRECIPITATION

UNCONFINED AQUIFER
 WATER LEVEL CONTOURS
 & LAKE ELEVATIONS
 FOR
 JULY 1975
 (FROM COMPUTER MODEL)



REFERENCE
 NORTH KENAI AREA MAP,
 PRODUCED FOR KENAI BOROUGH, 1968

INSUFFICIENT
LEGAL

1344

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

RECEIVED

JUN 4 1982

DRILLING LOG

Div. Of Geological Survey
Anchorage

Well Owner Union Chemical Use of Well Exploratory

Location (address of: Township, Range, Section, if known; or distance main road _____
1/2 mile North of Wellhouse 7m
Test Well 13/6

Size of casing 8" Depth of Hole 170 feet Cased to 160 feet

Static water level 50 ft. (~~above~~) (below) land surface. Finish of well (check one) open end ();

Screen (); Perforated ().

Describe screen or perforation N/A

Well pumping test at N/A gallons per (hour) (minute) for _____ hours with _____ ft. of drawdown from static level.

Date of completion April 11, 1982

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
0 TO 2	Casing <u>Stick up.</u>
2 TO 58	<u>Sandy Cobble Gravel.</u>
58 TO 70	<u>Sandy Gravel; Water Bearing.</u>
70 TO 75	<u>A/A: Silty.</u>
75 TO 99	<u>Grey Clay: Slightly Gravelly.</u>
99 TO 106	<u>Gravelly Clay: Sandy, Medium Hard</u>
106 TO 110	<u>Silty Sand: Gravelly.</u>
110 TO 112	<u>Grey Clay: Sandy, Soft.</u>
112 TO 115	<u>Sticky Clay.</u>
115 TO 135	<u>Sandy Clay: Semi, Consol.</u>
135 TO 140	<u>A/A, Wet & Heaving.</u>
140 TO 160	<u>Fine Sand: Silty, Wet-Heaves.</u>
160 TO <u>167</u>	<u>Very Fine Sand; Brown, Silty/ Clayey, Holds open hole.</u>
167 TO <u>170</u>	<u>Sandy Grey Clay.</u>
TO _____	_____

Wayne E. Nestor

NWWA Certified Contractor
Certificate No's. 814 & 873

INSUFFICIENT
LEGAL INFORMATION

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

RECEIVED 1345

JUN 4 1982

Div. Of Geological Survey,
Anchorage

DRILLING LOG

Well Owner Union Chemical 776-8121 Use of Well Commercial

Location (address of: Township, Range, Section, if known; or distance main road)
7m pump house

Size of casing 8" Depth of Hole 153'9" feet Cased to 150' feet

Static water level 48' ft. ~~(above)~~ (below) land surface. Finish of well (check one) open end ();

Screen (); Perforated ().

Describe screen or perforation

Well pumping test at _____ gallons per (hour) (minute) for _____ hours with _____ ft. of drawdown from static level.

Date of completion 3/15/82

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
<u>0 TO 2</u>	<u>Top soil</u>
<u>2 TO 13</u>	<u>Cemented gravel: some water brn, loose stratas w/6"-8" rocks at 10' level.</u>
<u>13 TO 44</u>	<u>Cemented gravel: brown, medium, hard & crumbles</u>
<u>44 TO 62</u>	<u>Sand & gravel: water bearing</u>
<u>62 TO 78</u>	<u>Sand & gravel: loose, caving, water bearing</u>
<u>78 TO 100</u>	<u>Clay: blue-grey some gravel</u>
<u>100 TO 103</u>	<u>Blue-grey clay</u>
<u>103 TO 105</u>	<u>Clayey gravel</u>
<u>105 TO 113</u>	<u>Silty sand & gravel: water bearing</u>
<u>113 TO 120</u>	<u>Very silty sand & gravel: water bearing</u>
<u>120 TO 125</u>	<u>Sand & gravel: heaving, cleaner, water bearing</u>
<u>125 TO 131</u>	<u>Silty sand & gravel; water bearing</u>
<u>131 TO 141</u>	<u>Silty sand & gravel: Clayey</u>
<u>141 TO 153</u>	<u>Fine silty sand</u>
<u>151 TO 153</u>	<u>Grey Clay</u>

Wayne E. Kesteven

NWNA Certified Contractor
Certificate No's. 814 & 873

Wayne E. Kesteven

NWNA Certified Contractor
Certificate No's. 814 & 873

1562 G

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

DRILLING LOG

Well Owner Union Chemical Use of Well COM

Location (address of: Township, Range, Section, if known; or distance main road)
Test Well 13/7 North of 7M

Size of casing 8 Depth of Hole 150 1/2 feet Cased to 150 1/2 feet

Static water level 59 ft. (~~above~~) (below) land surface. Finish of well (check one) open end (XXXX);

Screen () ; Perforated ()

Describe screen or perforation

TEST WELL

Well pumping test at _____ gallons per (hour) (minute) for _____ hours with _____ ft. of drawdown from static level.

Date of completion May 14, 1982

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
<u>0 TO 39</u>	<u>Dirt, Cobbels, Gravel</u>
<u>39 TO 40</u>	<u>Sand & Gravel - Very Little H2O</u>
<u>40 TO 44</u>	<u>Sand & Gravel, Clay, some H2O</u>
<u>44 TO 60</u>	<u>Sand & Gravel - H2O</u>
<u>60 TO 78</u>	<u>Sand & Gravel - Clean, Heaving H2O</u>
<u>78 TO 83</u>	<u>Grey Clay / Gravel</u>
<u>83 TO 90</u>	<u>Grey Gravelly Clay</u>
<u>90 TO 92</u>	<u>Grey Gravelly Clay - Medium Hard</u>
<u>92 TO 98</u>	<u>Grey Sandy Clay - Hard</u>
<u>98 TO 101</u>	<u>Grey Clay - Soft</u>
<u>101 TO 120</u>	<u>Grey Silty Clay - Soft</u>
<u>120 TO 140</u>	<u>Formation Gradually Clay - Sandy Clay - Very Silty Sand</u>
<u>140 TO 150</u>	<u>Very Silty Sand - Some Clay</u>
<u>TO</u>	
<u>TO</u>	

Wayne E. Kostley

AWWA Certified Contractor
Certificate No's. 814 & 873

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

* Log Rev. 10/25/85

state
5788

DRILLING LOG

Well Owner Union Chemical Use of Well Exploratory

Location (address of: Township, Range, Section, if known; or distance main road)
Test Well 13/4

Size of casing 8" Depth of Hole 160 feet Cased to *121.0* feet

Static water level *66.5* ft. (~~above~~) (below) land surface. Finish of well (check one) open end (X);

Screen (X); Perforated ().

Describe screen or perforation * 8" Tel. S.S. Screen 145 to 117 Top 2' Tight Wind, Bal. #25 slot

Well pumping test at *300* gallons per () (minute) for *24* hours with *38.8 ft. of drawdown from static level.

Date of completion January 15, 1982

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
<u>0 TO 2</u>	<u>Casing Stick up.</u>
<u>2 TO 23</u>	<u>Sandy Gravel: Semi Consol, Water @ 20'</u>
<u>23 TO 25</u>	<u>Sandy Gravel: Clayey.</u>
<u>25 TO 41</u>	<u>Sandy Gravel: Cemented, Water seaps in sand stringers.</u>
<u>41 TO 72</u>	<u>Gravelly Sand: loose, slightly clayey, Wet.</u>
<u>72 TO 81</u>	<u>Water Sand: Heaving, Slightly sandy.</u>
<u>81 TO 105</u>	<u>Grey Clay: Sticky, Slightly sandy.</u>
<u>105 TO 115</u>	<u>Gravel & Sand: Silty/Clayey, dense.</u>
<u>115 TO 147</u>	<u>Silty Sand & Gravel: wet (would not hold water from 127-147')</u>
<u>147 TO 160</u>	<u>Silty Grey Clay.</u>
<u>TO</u>	
<u>TO</u>	
<u>TO</u>	
<u>TO</u>	
<u>TO</u>	

[Handwritten Signature]
NITWA CONSULTING
Central, Nov 23 1982

1994

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

DRILLING LOG

No. of ...

LOCAL NO. 03D / -12-42 WAAH 1-17
USGS SITE ID 60404415/200501

Well Owner Union Chemical Use of Well Commercial

Location (address of: Township, Range, Section, if known; or distance main road _____)

Test Well 13/8 7N 12W 23

North of 7m 150-200 ft. N/W of 7p

Size of casing 6" Depth of Hole 151 feet Cased to 151 feet

Static water level 20¹⁸ ft. (above) (below) land surface. Finish of well (check one) open end ();

Screen (); Perforated (). 50.5 ft of sec 23 right on the 1/4 sec. line half way down

Describe screen or perforation None

Well pumping test at 0 gallons per (hour) (minute) for 0 hours with 0 ft. of drawdown from static level.

Date of completion June 23, 1982

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
-22 TO <u>20</u>	Casing Stick-up
0 TO <u>39</u> <u>37</u>	Sandy Cobble Gravel
<u>37</u> TO <u>60</u>	Sandy & Gravel (damp)
<u>60</u> TO <u>78</u>	Sand & Gravel
<u>78</u> TO <u>79</u>	Gray Clay
<u>79</u> TO <u>87</u>	Gray Gravelly Clay - Soft
<u>87</u> TO <u>89</u>	Gray Silty Clay - Medium Hard
<u>89</u> TO <u>101</u>	Variations of Gray Clay - Very Silty Sandy
<u>101</u> TO <u>103</u>	Silty Sand & Gravel (Formation Sample # 1)
<u>103</u> TO <u>109</u>	Silty Sand & Gravel (Formation Sample # 2)
<u>109</u> TO <u>111</u>	Silty Sand & Gravel (Formation Sample # 3)
<u>111</u> TO <u>113</u>	Silty Sand & Gravel (Formation Sample # 4)
<u>113</u> TO <u>138</u>	Silty Sand & Gravel (Formation Sample # 5-9)
<u>138</u> TO <u>151</u> <u>149</u>	Gray Clay, Dry. Open Hole Drilling Possible.
TO _____	

Wayne E. Westberg

NWWA Certified Contractor
Certificate No's. 814 & 873

Dave Rice 2-STATE

2599

M-W DRILLING, Inc.

SB 7-12-23 CDDC3-4 P.O. Box 10-378 • 10300 Old Seward Highway
712 26 BAAB (907) 349-8535
ANCHORAGE, ALASKA 99511

ROD GILGE

DRILLING LOG

1.2 mi OF
N KENAI RD
on Miller Loop Rd

Well Owner Union Chemical 776-8121 Use of Well Commercial

Location (address of: Township, Range, Section, if known; or distance main road)
400' north of 7M, Kenai, Alaska 13-9 production well

Size of casing 10" Depth of Hole ~~135~~ ¹³⁴ 140 feet Cased to 111.81 ^{109.81} feet BAAB

Static water level 65 ft. (above) (below) land surface. Finish of well (check one) open end () ;

Screen (); Perforated ().

*See as built

Describe screen or perforation *2 1/2" of 10" telescope Johnson 304 Stainless Steel screen w/2' trial pipe (6 5/8" OD) set from 136' to 140' varying slot sizes

Well pumping test at 520 gallons per (hour) (minute) for 20.75 hours with 35.5 ft. of drawdown from static level.

Date of completion October 21, 1982

started in Sept.

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
2 TO 0	Casing stickup
2 TO 4	Brown cemented gravel
4 TO 12	Gray silty gravel
12 TO 38	Gravelly with gray clay
38 TO 46	Gravel with gray clay, not so cemented
46 TO 52	Clean gravel
52 TO 82	Sand & gravel: heaving somewhat
82 TO 96	Gray clay with some sand and wood chips
96 TO 103	Gray clay with wood chips
103 TO 108	Clay with sand and small gravel; waterbearing
108 TO 133	Sand and gravel; waterbearing
133 TO 136	Sand and gravel with fine silty gray clay
134 TO 140	Sand, silt and clay
TO	
TO	

Handwritten signature and stamp
M-W DRILLING, Inc.
ANCHORAGE, ALASKA
Coordinator

LOCAL NO. SB7-12-23CDDC3-4
USGS SITE ID 604035151201302

no log

ADL# 40059*

owner: Better Concrete Products
(Kenai)

SB 7-12-27 ACA 1-9

USGS SITE ID 60401615121240
BORING AND WELL DATA LOCAL NO. 5800701227 ACA 1-9

Owner/ Boring or Well Number	Boring or Well Diameter (inches)	Maximum Depth Drilled (feet)	Original Surface Elevation M.S.L. (feet)	Static Water Table Elevation (feet)	Approximate Elevation of Screenable Water Bearing Soils		Test Well Screen Size			Maximum Production (gpm)	Test Well Drawdown (ft)	Specific Capacity (gpm/ft of drawdown)	Radial Influence of Well (ft.)	Coef. of Perm. (gals/day per sq.ft.)	Remarks
					Top (feet)	Bottom (feet)	Top Dia. (in.)	Length (ft.)	Slot Size (in.)						
ON SITE BORINGS AND WELLS															
Observation #1	6	140	132.5	+36.5	+18.5	-6.5	5-5/8	5	.018	--	2.2	--	--	--	Located 80 feet from TW 4
Observation #2	6	175	128.0	+38.0	--	--	--	--	--	--	--	--	--	--	
Observation #3	6	143	128.0	+36.5	+7	-12	5-5/8	5	.020	--	13.0	--	--	Located 30 feet from TW 4	
Observation #4	6	164	128.0	+33.5	-2	-8	--	--	--	--	--	--	--	--	
Observation #5	6	151	128.0	+40.5	+17	+3	5-5/8	5	.050	--	1.6	--	--	Located 30 feet from TW 3	
Observation #6	6	148	130.0	+39.0	+10	--	--	--	--	--	--	--	--	--	
Observation #7	6	137	134.0	+38.0	+19	+4	5-5/8	5	.018	--	1.0	--	--	Located 50 feet from TW 2	
Observation #8	6	120	130.0	+39.0	+18	--	5-5/8	5	.018	--	1.3	--	--	Located 30 feet from TW 2	
Test Well 1	10	135	128.0	+38.0	--	--	--	--	--	NG (not tested)--	--	--	--	--	
Test Well 2	10	130	133.0	+35.0	+19	+6	9-5/8	3	.050 10 .016	94	27.5	3.4	100-150	214	Radius of influence extrapolated
Test Well 3	10	122	129.0	+39.0	+25	+11	9-5/8	5	.050 6 3 .020	104 104 104	28.5	3.6	100-150	218	Radius of influence extrapolated
Test Well 4	10	146	129.5	+35.5	+5.5	-14.5	9-5/8	20	.018	183	47.0	3.9	100	194	Radius of influence extrapolated
VICINITY BORINGS AND WELLS															
Standard Oil(1) (2) (3)	6	171	150±	+26	+2	-21	5-5/8	10 10	.010 .014	100	10	10.0	--	--	Wells 1 and 3 reportedly same as 2. Water has high iron content.
Chugach Electric (1) (2) (3)	10 10 10	173 173 183	150± 150± 150±	+28 +28 +28	-13 -13 -12	-- -- --	9-5/8 9-5/8 9-5/8	10 10 10	.010 .010 .010	60 60 150	14 16 --	4.3 3.8 --	-- -- --	-- -- --	Reportedly started pumping hot water after earthquake. This well was acidified in 1965 when screen became clogged. Water has high iron content.
Rig Tenders (1) (2) (3) (4)	6 10 10 10	200 60 70 80	30 30 30 30	+19 +10 +15 +12	-25 -10 -22 -3	-40 -18 -30 -16	5-5/8 5-5/8 9-5/8 9-5/8	5 10 8 13	.014 .020 .012 .012	135 200 100 --	22 38 28 --	6.1 5.3 3.6 --	-- -- -- --	-- -- -- --	Water high in iron. Same as above. Same as above. Pump test not completed to date.
Phillips Petroleum (1) (2) (3) (4)	6 6 6 6	245 287 -- 245	115± 132± -- --	+72 -- -- --	+72 +38 -- --	+38 +31 -- --	-- -- -- --	-- -- -- --	-- -- -- --	800-1000 (est.) N.G. N.G. 600-800 (est.)	-- -- -- --	-- -- -- --	-- -- -- --	-- -- -- --	No pump test to date. Water high in iron. Not tested. Not tested. Not tested. Not tested.
Kenai Pipeline	6	79	135±	+96	+67	+56	5-5/8	10	.020	70	7	10.0	--	--	Red brass screen used.
Cement Plant	8	69	118± M.S.L. 130±	+80	+75	+65	7-5/8	10	.030	150	--	--	--	--	Water high in iron.
Tea Pee	6		130±	--	-80	-81	Perforated Casing			4	--	--	--	--	Took two weeks of pumping to clear water.

* case closed 9/12/80 for lack of H₂O use in last 5 years
however well is still functioning.

NOTES:

1. THE FIGURE NEXT TO THE WELL LOCATION INDICATES THE WELL YIELD
2. NG INDICATES THAT THE CONDITIONS ENCOUNTERED IN THE BORING ARE NOT SUITABLE FOR WELL DEVELOPMENT
3. ON-SITE WELL DATA HAS BEEN ESTABLISHED BY RECORDS TAKEN UNDER DAMES & MOORE SUPERVISION.
4. VICINITY WELL DATA WAS OBTAINED FROM VARIOUS SOURCES, VERBALLY AND IN WRITING. THIS INFORMATION MAY NOT REFLECT A HIGH DEGREE OF ACCURACY BUT SHOULD INDICATE GENERAL CONDITIONS.
5. ESTIMATES OF POTENTIAL YIELD OF BORINGS ARE BASED ON INTERPRETATION OF BORING INFORMATION. ACTUAL YIELDS MAY VARY CONSIDERABLY FROM THE ESTIMATES.
6. REFER TO THE WELL INVESTIGATION PLAN, PLATE 2, FOR ADDITIONAL LOCATION INFORMATION OF OBSERVATION AND TEST WELLS.
7. REFER TO THE APPENDIX FOR STAGE PUMP TEST DATA FOR ON-SITE WELLS.

location see following page

DATA SUMMARY

WELLS AND EXPLORATIONS AT THE SITE AND IN THE VICINITY OF THE SITE

SB 7-12-27 ACA 1-9

LOCAL # SB 6-12-14-AACC 1-7
SITE ID 60420715/193101

SGS SITE ID LOCAL NO. SB 7-12-14A ~~ADD~~ CC 672
(ADL 00148)

got ADL #
from John
in Kenai DNR
office

Post Office Box 158
Kenai, Alaska 99611
June 7, 1977

Douglas Olson
Post Office Box 58
Kenai, Alaska 99611

Dear Mr. Olson:

Block 1 GOVT LOT 3

The following is a log of the well dug on your Island Lake
property, Lake Shore Estates, Lot 13, E 1/4 NW 1/4 NE 1/4 Section
1/4 Township 7N Range 12W Seward Meridian. ↑ wrong

5/27/77	0-31'	0-12'	Gravel
		12-14'	Gravel & small amount of clay
		15-31'	Gravel
		31'	water
5/28/77	31-36'	31-36'	water with gravel
		36'	finished here in order to have a 5' head of water.

ramped over an hour at 15 gallons
a minute and the well never went
dry.

Thank you very much for the opportunity to be of service.

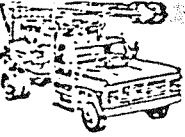
Yours very truly,

DARC Enterprises

Rex D. Bennett

RDL/cab

CUSTOMER'S COPY



13635

WS & S. Co.

WATER SYSTEMS & SERVICE

Rt. 1, Box 1517

Kenai, Alaska 99611



Dated this 29th day of June, 1987

~~Vial Construction~~
Box 8306 MRB
Kenai, AK 99611

Owner: John + Debra Yanak

Dear Sir:

The following is a well log located on Lot 1 Block 1
BELUGA SHORES No 2
in the Kenai Recording District. The owner at the time
water well was requested TIM VEHK.

0	to	3	feet	topsoil
3	to	33	feet	gravel no water
33	to	43	feet	sand and gravel water formation
	to		feet	

Submersible pump was wasn't installed as requested
Screen wasn't installed as requested and/or necessary
Well yield wasn't tested by pumping, bailing at 20 gpm

We have been pleased to serve your water needs and if you
have any further questions, problems, or comments please
don't hesitate to call or write.

Sincerely,

KENNETH D. DYER
Owner

kd/dd

LAS 9768

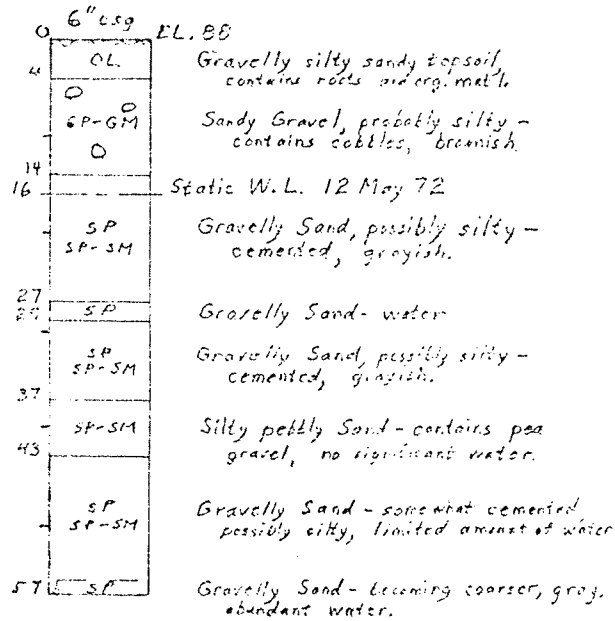


cc: D665 11/86

SB 07 - 12 - 26 DBAA

WELL - BERNICE LAKE CAMPGROUND

SW $\frac{1}{4}$ of SE $\frac{1}{4}$ of Sec. 15, T 7 N, R 12 W, S. M.



Well drilled 10-12 May 1972

by Alaskan Enterprises (Floyd Howell, driller).

Open end casing. Well developed by cleaning out with a sand pump, then bailing until bottom stabilized at lower end of casing. Well was pumped at 20 gpm for an hour - water discharged clean, with only a few scattered sand grains.

Bail-tested at 30 gpm, 5 ft. drawdown.

SB 7-12-15 DCBC 1-4
604133151214801

NK20

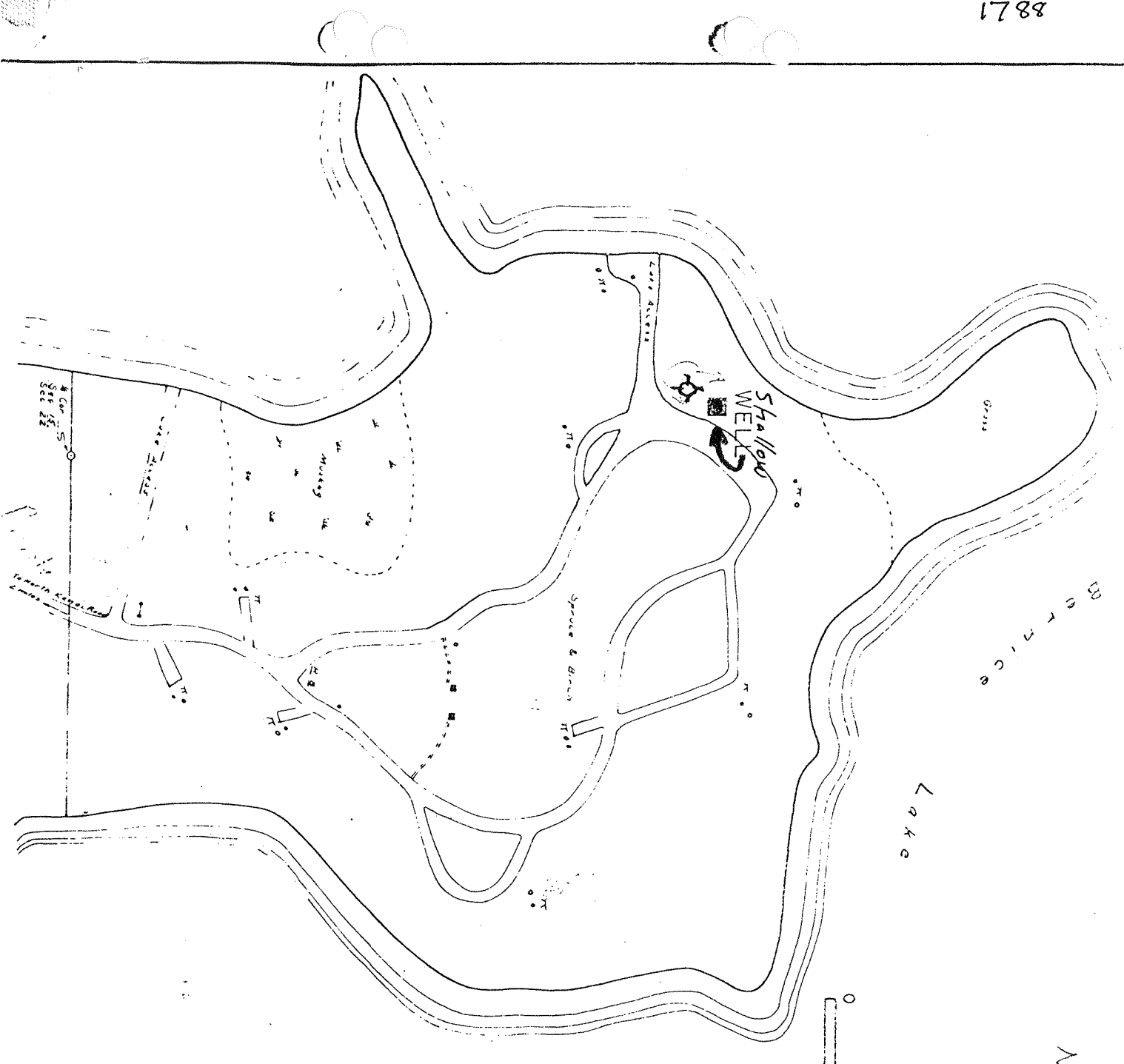
BERNICE LAKE CAMPGROUND

Lot 6, Section 15, T.1N, R.12W, S.1M.
2.35 Acres
June 1962
Drawn by - A.O. 507



- Legend**
- Brass Cap Monument
 - Campground Boundary
 - Entrance Sign
 - Table
 - Fireplace
 - Trailer
 - Registry Box
 - Bulletin Board
 - Trash Barrel
 - Timber Type Line
 - Roads
 - Foot Trail
 - Muskeg
 - Lake Shore

⊕ deep well
 □ shallow well



INSUFFICIENT
LEGAL INFORMATION

1343

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

RECEIVED

DRILLING LOG

Div. Of Geology and Surveying
Use of Well Commercial

Well Owner Union Chemical

Location (address of: Township, Range, Section, if known; or distance main road _____)

Well # 13/2-8

Size of casing 8" Depth of Hole 153 feet Cased to 153 feet

Static water level 70 ft. (~~above~~) (below) land surface. Finish of well (check one) open end (X) ;

Screen () ; Perforated ().

Describe screen or perforation None

Well pumping test at _____ gallons per (hour) (minute) for _____ hours with _____ ft. of drawdown from static level.

Date of completion November 24, 1981 Well abandoned for insufficient yield

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
0 TO 2	Casing stickup
2 TO 10	Tan silty gravel
10 TO 45	Brown silty gravel (damp)
45 TO 67	Sand and gravel (damp)
67 TO 80	Gray clay and gravel
80 TO 84	Sand and gravel (damp)
84 TO 98	Gray clay with traces of gravel
98 TO 99	Gray clay sand and gravel (damp)
99 TO 102	Sand, clay and gravel (damp)
102 TO 104	Sand and gravel (damp)
104 TO 106	Silty sand clay, waterbearing
106 TO 109	Wet silty sand
109 TO 112	Silty sand, some gravel, waterbearing
112 TO 113	Wet sand and gravel
113 TO 115	Wet sand and gravel

Wayne E. Wesley
NWWA Certified Contractor
Certificate No's. 814 & 873

776-8121
Union
Chemical

INSUFFICIENT
LEGAL INFORMATION

1343

M-W DRILLING, Inc.

P. O. Box 4-1224 • 1310C International Airport Road
(907) 274-4611
ANCHORAGE, ALASKA 99509

DRILLING LOG

Well Owner Union Chemical (page 22) Use of Well Commercial

Location (address of: Township, Range, Section, if known; or distance main road _____

Size of casing _____ Depth of Hole _____ feet Cased to _____

Static water level _____ ft. (above) (below) land surface. Finish

Screen () ; Perforated ()

Describe screen or perforation _____

Well pumping test at _____ gallons per (hour) (minute) for _____
of drawdown from static level.

Date of completion _____

CONTINUATION

() ;

ft.

WELL LOG

Depth in feet from ground surface	Give details of formations penetrated, size of material, color and hardness
115 TO 117	Wet gravel
117 TO 127	Gray silty sand, waterbearing
127 TO 138	Gray silty clay, some gravel, waterbearing
138 TO 140	Gray silty sand w/traces of gravel, waterbearing
140 TO ¹⁵¹ 153	Gray silty sand and gravel, waterbearing
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	
TO	

Wayne E. Westberg

NWWA Certified Contractor
Certificate No's. 814 & 973

SOLDOTNA DRILLING CO.

WATER WELL CONTRACTORS

P. O. Box 351

SOLDOTNA, ALASKA 99669

OCT 3 1974 DJW

DATE October 3 19 74

Collier Carbon & Chemical Corporation

Well Logs for Test Bores

Test Bore # 8				
0'	12'	Silty Sand & Gravel		
12'	34'	Gravelly Sand		
34'	58'	Sandy Gravel--Slightly Cemented		
58'	66'	Silty Fine Sand		
66'	70'	Fine Sand w/Lignite chunks--water		
Test Bore #9				
0'	31'	Gravelly Sand		
31'	56'	Sandy Gravel--cemented		
56'	64'	Sand w/Lignite bits		
64'	70'	Fine Sand--water		
Test Bore #10				
0'	10'	Gravelly Silty Sand		
10'	30'	Gravelly Sand		
30'	62'	Sandy Gravel--Cemented		
62'	70'	Fine Silty Sand w/Lignite--water		
Test Bore #11				
0'	4'	Top Soil		
4'	36'	Gravelly Sand		
36'	69'	Sandy Gravel		
69'	75'	Fine Silty Sand--water		
Test Bore #12				
0'	4'	Top Soil		
4'	35'	Gravelly Sand		
35'	61'	Sandy Gravel		
61'	70'	Med.-Coarse Sand		
70'	75'	Fine Silty Sand--water		

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OLD DOTNA DRILLING CO
WATER WELL CONTRACTORS
 P. O. Box 251
 SOLDOTNA, ALASKA 99669

DATE August 28 1974

Well Logs for Test Borings

#1 Test Bore		
0	31'	Gravelly Sand
31'	48'	Sandy Gravel--partially cemented with iron oxide--reddish brown
48'	61'	Gray sand & Lignite Particle
61'	66'	Silty Sand
66'	73'	Fine Sand--water bearing
73'	6"	Clay--Blue Gray
#2 Test Bore		
0	27'	Gravelly Sand
27	55	Sandy Gravel--Cemented--Red-Brown
55	63	Sand w/lignite Particale
63	71	Med. to course sand-water
#3 Test Bore		
0	36'	Gravelly Sand
36	57'	Sandy Gravel--Cemented--Red
57	64	Sand & Lignite
64	70	Water Bearing fine Sand
71		Solid Clay
Test #4 Bore		
0	6'	Over burden Soil
6	34	Gravelly Sand
34	46	Sandy Gravel--Partly cemented
46	61	Grey Sand--Small gravels & Lignite bits
61	72	Fine Sand--greyish Water
73		Clay Blue Grey

SOLDOTNA DRILLING CO
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Well Logs for Test Bores

Test Bore # 8						
0'	12'	Silty Sand & Gravel				
12'	34'	Gravelly Sand				
34'	58'	Sandy Gravel--Slightly Cemented				
58'	66'	Silty Fine Sand				
66'	70'	Fine Sand w/Lignite chunks--water				
Test Bore #9						
0'	31'	Gravelly Sand				
31'	56'	Sandy Gravel--cemented				
56'	64'	Sand w/Lignite bits				
64'	70'	Fine Sand--water				
Test Bore #10						
0'	10'	Gravelly Silty Sand				
10'	30'	Gravelly Sand				
30'	62'	Sandy Gravel--Cemented				
62'	70'	Fine Silty Sand w/Lignite--water				
Test Bore #11						
0'	4'	Top Soil				
4'	36'	Gravelly Sand				
36'	69'	Sandy Gravel				
69'	75'	Fine Silty Sand--water				
Test Bore #12						
0'	4'	Top Soil				
4'	35'	Gravelly Sand				
35'	61'	Sandy Gravel				
61'	70'	Med.-Coarse Sand				
70'	75'	Fine Silty Sand--water				

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SOLDOTNA DRILLING CO.
WATER WELL CONTRACTORS
 P. O. Box 351
 SOLDOTNA, ALASKA 99669

DATE August 28 1971

Well Logs for Test Borings

#1 Test Bore				
0	31'	Gravelly Sand		
31'	48'	Sandy Gravel--partially cemented with iron oxide--reddish brown		
48'	61'	Gray sand & Lignite Particle		
61'	66'	Silty Sand		
66'	73'	Fine Sand--water bearing		
73'	6"	Clay--Blue Gray		
#2 Test Bore				
0	27'	Gravelly Sand		
27'	55'	Sandy Gravel--Cemented-Red-Brown		
55'	63'	Sand W/lignite Particals		
63'	71'	Med. to course sand-water		
# 3. Test Bore				
0	36'	Gravelly Sand		
36'	57'	Sandy Gravel--Cemented--Red		
57'	64'	Sand & Lignite		
64'	70'	Water Bearing fine Sand		
71'		Solid Clay		
Test #4 Bore				
0	6'	Over burden Soil		
6'	34'	Gravelly Sand		
34'	46'	Sandy Gravel--Partly cemented		
46'	61'	Grey Sand--Small gravels & Lignite bits		
61'	72'	Fine Sand--greyish Water		
73'		Clay Blue Grey		

